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RESISTORS, VARIABLE

(FILM TYPE)

QUARTERLY PROGRESS REPORT #14

1 SEPTEMBER THROUGH 30 NOVEMBER 1961

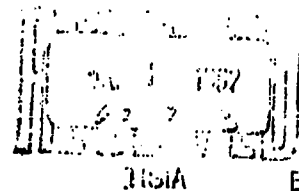
CONTRACT NO. DA-36-039-SC-75981
ORDER NO. 43796-PP-58-81-81

Prepared for the U. S. Army Signal Agency

by

ENGINEERING AND RESEARCH DIVISION

INTERNATIONAL RESISTANCE COMPANY



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RESISTORS, VARIABLE

(FILM TYPE)

QUARTERLY PROGRESS REPORT #14

1 SEPTEMBER THROUGH 30 NOVEMBER 1961

Contract No: DA 36-039-SC 75981-
Order No: 43796 PP-58-81-81
Applicable Specification: M.L. R. 94B (Modified)
Report Prepared at: International Resistance Co.
401 North Broad Street
Philadelphia 8, Penna.
Prepared By:

John Woods
Senior Product Development Engineer

Approved By:

Harry Casey
Project Leader



Sava I. Sherr
Manager, Government Operations

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ABSTRACT

Acceptable RV12 substrates have been received from American Lava.

Pre-pre-production tests and subsequent results obtained with unhoused elements show that moisture resistance can be improved with a thin film coating or a slight revision in termination material. Moisture failures appear to be greatly reduced by running the test without housings; indicating that moisture entrapment in the housings has been a major hindrance to good performance.

Manicuring of facilities continues as required.

An improved method of applying the silver shorting path for "C" tapers, which involves spraying through a mask in place of the silk screening method now used, has been developed.

BACKGROUND

The purpose of this contract is to develop, design, procure, install and maintain manufacturing facilities to produce variable film-type resistors capable of satisfying MIL-R 94B (as modified in accordance with Contract No. DA-36-039-SC-75981) whose major characteristics include 125°C ambient temperature, 100,000 cycle operation at ambient with rated load, and improved environmental stability.

In a Technical Action Request dated July 18, 1959, RC proposed changes in the applicable components specifications. Subsequently, with one exception, the requested changes were approved. The exception involved rotational life characteristics and the possibility of future approval was made contingent upon the submission by RC of further technical information. The most significant change involved noise level before and after rotation. This ENR level must (1) not exceed 1% of total resistance or 5 ohms (whichever is greater), (2) nor may it exceed 5% of total resistance or 25 ohms (whichever is greater), after 100,000 cycle operation, full rated load at 125°C or de-rated load at 150°C.

As a result of the signing of an operation agreement between IRC and Chicago Telephone Supply Service of Elkhart, Indiana, it was decided that IRC and CTS would submit a proposal to the USASSA allowing establishment of facilities at CTS.

The development program to date has been directed toward the establishment of a system (substrate, film and contact) which is capable of meeting the contract requirements. After considerable effort, this system has been incorporated into a potentiometer design.

Carbon alloy, metal, and glaze films have been tested on ceramic substrates using molded carbons, precious metals and carbongraphite wiper materials. While both metal film and resistive glaze elements showed some promise, the performance levels were not as high as those observed for carbon alloy.

After considerable difficulty experienced by Coors Porcelain Company in making substrates in the designed configuration, another vendor (American Lava) has tooled to produce 96% alumina substrates for both the RV11 and RV12 potentiometers. The surface finish requirement of these

substrates has been established at 15 microinches, and carbon alloy has been selected for deposition on the substrates. A single grade of carbon (Pure Carbon Co. E-27) will be used as the wiper on all resistance ranges from 100 ohms through 1,000,000 ohms.

The method of adjusting resistance tolerance as reported in Quarterly Report #7, on production elements is operational. The screening of a pattern of conductive material to produce nonlinear taper has been proved feasible.

Temperature coefficient curves indicate that for linear elements, 750 PPM can be maintained for resistance of 100,000 ohms and less. At 200,000 ohms, 750 PPM becomes marginal and 1500 PPM is exceeded for all values of 400,000 ohms and greater. Temperature coefficient on "C" tapered elements will correspond to those values observed on linear elements which are approximately double the resistance range of the tapered element.

An improved termination of VZA conductive paint with a VLS carbon ink overlay provides moisture resistance superior to that of VZA alone. However, moisture tests of housed elements have shown a high failure rate, indicating that the sealed housing has a deleterious effect.

I. PRODUCT ENGINEERING

A. Substrates

Deliveries of 1500 RV12 substrates have been received from American Lava. Dimensions are acceptable with the following deviations noted: 1) the $.968 \pm .005$ outside diameter is undersized on most pieces, measuring .956 to .959; 2) the inner wall in the terminal slot area has been made thicker by addition of a radial contour, whereas, the drawing specifies two chords of the inside diameter. Deviation 1) has been accepted after checking with CTS to confirm that the substrate can be clinched in the clinching ring; 2) is a minor deviation having no effect on processing or assembling the element.

A small lot (271) of RV11 substrates were rejected, and returned to vendor, for high surface roughness. A sample of six pieces averaged 19.4 microinch RMS with a span of 18 to 22 microinch.

B. Testing

The pre-pre-production tests, representing the first data obtained with the carbon alloy elements assembled in housings, have been completed. Most of the data was reported in Quarterly Report #13. The completed data summaries are presented here (Tables II through V.). As previously noted, load life and rotational life changes were greater than the specified $\pm 5\% \Delta R$. Some of the larger load-life changes were attributed to substrate and termination defects. Process changes have been made to correct these conditions. Because one lot each of RV11 and RV12 units was found to have been improperly mounted on heat sinks during the load life test, the test was repeated (test lots No. 14200 and 14201 in Table II) with potentiometers assembled at the same time as those previously tested. The resistance changes were again high. Disassembly of the units having the greatest changes showed that the terminations were thin and incomplete, as was noted before.

Another defect visible in the RV12 pots is an inadequate crimping of the clinching ring which prevents proper seating of the substrate against the ring. This decreases the heat conduction to the housing causing excessive film temperature. CTS will be advised of the situation so that corrections can be made before pre-production.

The major problem which showed up in pre-pre production testing was poor performance in the moisture resistance test.

Data obtained in the last quarter (Quarterly Progress Report #13) indicated that a carbon ink overlay covering the VZA termination would improve moisture resistance. A lot of 12 RV11 potentiometers were assembled with the improved termination. All openings in the housing were sealed with epoxy; and in four assemblies, the opening between the shaft and bushing was also sealed. The latter operation prevents rotation of the shaft, but was used in this instance to determine whether or not an improved shaft seal is necessary. Half of the pots were submitted to the MIL-R-94B moisture resistance test at IRC; and half at CTS.

All of the units which had been sealed around the shaft, and 4 of the 8 other units, were "open" after 10 moisture cycles. (See Table I)

In an effort to improve moisture resistance of the element itself, 10 groups of unhoused elements were prepared and submitted to the moisture test. These groups used various protective coatings and termination modifications, as shown in Table VII. This table also summarizes the test results after 10 moisture cycles. Group numbers 4, 5, 8, 9, and 10 had no failures. There were no "opens" in any group, including group 6 which was terminated in the same manner as were the assembled pots of Table I. Moisture cycling of the unhoused elements is continuing in order to determine the best system.

It is apparent from the findings to date that the sealed housing is a detriment to good moisture resistance. In future assemblies, the housing will be left completely unsealed to allow entrapped moisture to escape.

II. PRE-PRODUCTION

Production of elements was stopped pending evaluation and solution of the moisture problem. Manufacture of pre-production elements will be started, using the revised termination and/or coating indicated by the tests in i B. above.

"C" taper shorting patterns have been successfully screened. Because of the fine resolution required in the RVII pattern, the consistency of the VZA is critical, and the screen must be cleaned frequently.

III. FACILITIES

A. Element

The element facility changes during the past quarter consisted of some minor mancuring of the equipment and the development of an improved technique for applying the taper shorting path.

The screening set-up for tapers was brought to the point where the taper pattern could be screened on the elements consistently. As pointed out above, the screening material viscosity is critical, however, the system is workable.

An alternative method of applying the same pattern was developed. It was demonstrated that a mask could be made by the photo-etch process which retained sharp definition. The silver was sprayed through this mask and the resulting pattern was acceptable. The operation is less critical than screening so this method will be tooled.

A checking fixture for reading resistance at the mid rotation point of the elements was made.

Also, an improved contactor of Pallinoy #7 Alloy was made to monitor the resistance of an element while adjusting it on the machine.

B.

Housing

No changes to report.

CONCLUSIONS

1. Acceptable substrates can be produced for both the RV11 and RV12 sizes.
2. Moisture results obtained with unboxed elements are superior to data obtained with assembled, epoxy-sealed potentiometers.
3. Definition and ease of application of the "C" taper pattern are improved by the use of a photo-etched mask and spray in place of the silk screening process.

PROGRAM FOR NEXT QUARTER

1. The moisture tests on unhoused elements will be continued to determine which termination and/or coating provides the most protection.
2. Pre-production of elements will be begun using the indicated new termination.

PERSONNEL

<u>Engineering</u>	<u>Hours</u>
J. Woods	136.0
M. Steidlitz	58.5
<u>Mechanical, Chemical, Electrical Development</u>	
F. Surowiec	21.0
E. Dietrich	15.0
E. Altorfer	2.0
W. Gold	20.0
<u>Technicians</u>	
B. Kelly	157.5
O. Leidic	66.5
A. Graft	40.0
G. Williams	40.0
D. Terry	136.5
E. Greenleaf	76.0
T. Arline	40.0
<u>Test Section</u>	<u>124.7</u>
Total IRC	933.7
Total CTS	<u>44.0</u>
TOTAL	977.7

APPEND X

<u>TABLE</u>	<u>PAGE</u>
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TABLE I

Moisture resistance tests of 325K Ω RVII potentiometers (combined IRC and CTS results).

No. Units	(% Δ R (spec: $\pm 5\%$))			Fail	Remarks
	Max	Min.	Ave.		
8	+4.6	+0.81	+2.05 (ave. of 4)	4/8 (4 "open")	Units epoxy sealed on back of element and between case and bushing
4	ALL UNITS "OPEN"			4/4	Units sealed as above, plus epoxy seal around shaft.

Note: All units passed 500 V AC dielectric strength; 1/12 failed insulation resistance: 40 M Ω (spec. 100 M Ω minimum).

3-303-1

PREPARED BY AK, JW		TITLE		PRE-PRODUCTION TESTS - FILM POTENTIAL									
CHECKED BY		185KΩ											
APPROVED BY													
RESISTANCE & DATA NO.		TEMPERATURE COEFFICIENT SPEC: 7500mV/C					SPEC: 1.34% 1.76% 2.16% MAX LOAD LIFE 125°C ± 150°C				SPEC: 1.34% 1.76% 2.16% MAX		
		COEFFICIENT					LOAD LIFE						
		PPM/°C -15°C	PPM/°C -55°C	PPM/°C +25°C	PPM/°C +105°C	PPM/°C +165°C	%ΔR 96 HRS	%ΔR 192 HRS	%ΔR 528 HRS	%ΔR 1008 HRS			
FILM POT. (1PG) RV-11 185KΩ 1/2W 08227	AV	-947	-872	-722	-704	-684	+0.34	+0.50	+0.77	+0.71	125°C FULL LOAD		
	SPAN	-232	-774	-653	-629	-603	+0.32	+0.23	+1.06	+1.11			
	FAIL	-998	-916	-788	-763	-746	+0.35	+0.60	+0.65	+0.46			
		4	4	4	4	4	4	4	4	4			
FILM POT. (1PG) RV-11 185KΩ 1/2W 08228	AV	-844	-785	-663	-636	-612	+0.34	+0.44	+1.19	+0.57	150°C 40% LOAD		
	SPAN	-790	-731	-613	-585	-555	+0.42	+0.52	+0.80	+1.40			
	FAIL	-790	-863	-555	-711	-697	-0.50	-0.50	-3.32	+0.07			
		4	4	4	4	4	4	4	4	4			
FILM POT. (1PG) RV-11 185KΩ 1/2W 08229	AV										150°C 40% LOAD		
	SPAN												
	FAIL												
FILM POT. (1PG) RV-11 185KΩ 1/2W 08230	AV										150°C 40% LOAD		
	SPAN												
	FAIL												
	AV										150°C 40% LOAD		
	SPAN												
	FAIL												
	AV										150°C 40% LOAD		
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	SPAN												
	FAIL												

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PREPARED BY <i>RK, 1W</i>		TITLE <i>PRE-PRODUCTION TESTS</i>				TYPE <i>RV11 RV12</i>		DWG. NO. <i>B</i>		TABLE <i>III</i>	
CHECKED BY								DATE <i>9-18-61</i>			
APPROVED BY											
RESISTANCE & DATA NO.		TEMPERATURE COEFFICIENT <small>RV11: 150 PPM TO 250K & 150 PPM TO 175K RV12: 750 PPM TO 500K & 750 PPM TO 175K</small>					LOAD LIFE SPEC: 15%				
		-15°C PPM	-25°C PPM	+125°C PPM	+175°C PPM	+650°C PPM	26 HRS	192 HRS	504 HRS	1008 HRS	TEMP LOAD
<i>RV12 2W 70KΩ 11120</i>	AV	-362	-362	-315	-318	-304	+4.25	+3.99	+3.5	+20.6	
	SPAN	-380	-383	-335	-329	-321	+9.93	+9.44	+7.24	+58.74	150°C
	FAIL	-353	-348	-290	-306	-282	+1.31	+1.11	+1.39	+1.35	0.2W
<i>RV11 1/2W 1PC. 350KΩ 11296</i>	AV	-1643	-1762	-1191	-1173	-1051	+1.69	+0.98	+2.89	+2.93	
	SPAN	-1750	-1888	-1290	-1253	-1106	+1.98	+1.21	+2.71	+3.68	150°C
	FAIL	-1508	-1664	-1095	-1074	-956	+1.49	+0.72	+2.17	+2.46	0.2W
<i>RV11 1/2W 3PC. 250KΩ 11121</i>	AV	-1125	-1205	-851	-888	-902	+4.77	+4.0	+5.65	+14.93	
	SPAN	-1138	-1224	-880	-898	-936	+8.62	+7.36	+7.14	+24.21	150°C
	FAIL	-1118	-1194	-828	-875	-864	+0.85	+0.63	+1.05	+5.45	0.2W
<i>RV12 2W 70KΩ 11118</i>	AV	-349	-341	-344	-342	-349	+1.16	+4.10	+4.35	+5.65	
	SPAN	-365	-365	-368	-355	-372	+6.30	+5.91	+9.34	+12.48	125°C
	FAIL	-283	-296	-325	-326	-326	+1.19	+1.34	+1.46	+4.08	FULL
<i>RV11 1/2W 1PC. 350KΩ 11297</i>	AV	-1646	-1728	-1135	-1151	-1025	+3.70	+4.95	+11.16	+11.16	
	SPAN	-1507	-1604	-1220	-1213	-1173	+8.26	+10.74	+17.87	+21.17	125°C
	FAIL	-1522	-1556	-1025	-1064	-1064	+0.42	+0.91	+4.45	+4.45	FULL
<i>RV11 1/2W 2PC. 350KΩ 11119</i>	AV	-1131	-1176	-822	-888	-770	+2.86	+6.52	+6.76	+11.46	
	SPAN	-1158	-1224	-975	-934	-844	+4.99	+8.45	+8.42	+13.75	125°C
	FAIL	-1085	-1129	-825	-835	-836	+0.45	+5.54	+5.11	+7.57	FULL
<i>RV12 2W 70KΩ 12901</i>	AV	-	-	-	-	-	+3.40	+3.91	+8.45	+11.16	
	SPAN	-	-	-	-	-	+5.57	+6.39	+11.52	+11.52	125°C
	FAIL	-	-	-	-	-	+1.10	+1.17	+2.44	+2.44	FULL
<i>RV11 1/2W 350KΩ 14100</i>	AV	-	-	-	-	-	+3.55	+6.80	+8.86	+10.41	
	SPAN	-	-	-	-	-	+1.11	+12.17	+12.17	+27.21	125°C
	FAIL	-	-	-	-	-	+0.17	+3	+12.33	+11.77	FULL
<i>RV12 2W 70KΩ 14201</i>	AV	-	-	-	-	-	+2.85	+1.44	+5.64	+7.73	
	SPAN	-	-	-	-	-	+3.18	+4.00	+12.61	+17.22	125°C
	FAIL	-	-	-	-	-	+0.18	+0.25	+0.25	+0.74	FULL
	AV										
	SPAN										
	FAIL										
	AV										
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	SPAN										
	FAIL										
	AV										
	SPAN										
	FAIL										

① ONE UNIT OPEN; NOT IN AVE.
ON SPAN

- NOTE:-
1. FAILURE RATE FOR TC ON RV11, 250KΩ ASSUMES 1500 PPM SPEC.
 2. UNITS OF #11297 & 12901 NOT PROPERLY MOUNTED ON HEAT SINK.

X 3-303-1

PREPARED BY BK, JN		TITLE PRE-PRODUCTION TESTS		TYPE RV11 RV12		DWG. NO. B		TABLE IV	
CHECKED BY						DATE		9-18-61	
APPROVED BY									
RESISTANCE & SPEC DATA NO.		VIBRATION TESTS MAX		MOISTURE					
		RV11-1.5%	RV12-1.5%	± 5%	100M2				
		900K 900K	900K 900K	MINI. TEST	DIELECTRIC	INSUL. RES			
		TOTAL 50%	900K			MEG. Ω			
RV12 2W	AV	± 0.17	± 0.18	± 6.90		12.71x10 ²			
90K-2	SPAN	+ 0.44	+ 0.42	117.57		30x10 ²			
11110	FAIL	+ 0.06	+ 0.20	- 0.66		14.71x10 ²			
		0	0	0	0	0	0	0	0
RV11-1 PL	AV	± 0.07	+ 0.86	ALL					
1/2 W	SPAN	+ 0.25	+ 5.29	OPEN					
350K-2	FAIL	+ 0.06	+ 0.81						
11294		0	0	0	0				
RV11-2 PL	AV	+ 0.27	± 0.57	+ 3.66		165.6x10 ²			
3/4 W 250K-2	SPAN	+ 0.26	10.09	+ 6.34		500x10 ²			
11111	FAIL	+ 0.15	- 1.20	+ 0.98		4.5x10 ²			
		0	0	3 ③ 4	0	4	0	4	4
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① = NO. CIRCLES NOT INCL.
IN AVE OR MAX.

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PREPARED BY BK, JN			TITLE PRE-PRODUCTION TESTS				TYPE RV11 RV12		DWG. NO. B		TABLE V	
CHECKED BY									DATE		9-18-61	
APPROVED BY												
RESISTANCE & SPEC. DATA NO.		SOLDER	ROTATION, FL @ 125°C									
		±2%	18R _T	5%R _T	±5%							
		%DR	ENR INT %R _T	ENR INT %R _T	%DR							
RV12 2W	AV	+0.10	0.34	1.19	+4.38							
70K Ω	SPAN	+0.52	0.51	2.56	+6.93							
2 \pm 0Z.		0	0.27	0.54	+1.39							
11106	FAIL	0	0	0	2							
RV12 2W	AV	+0.05	1.16	3.16	+4.99							
70K Ω	SPAN	+0.06	3.2	3.90	+7.12							
1 \pm 0Z.		0	0.2	2.64	+2.62							
11107	FAIL	0	0	1	2							
RV11 1/2W	AV	+0.27	0.60	0.55	+4.75							
1PC	SPAN	+0.47	0.89	1.06	+6.07							
350K Ω		-0.18	0.49	0.16	+3.00							
1 \pm 0Z.	FAIL	0	0	0	2							
11109		0	0	0	4							
RV11 1/2W	AV	+0.23	0.64	1.0	+6.53							
1PC	SPAN	+0.32	0.91	2.31	+10.34							
350K Ω		+0.06	0.38	0.25	+3.43							
1 \pm 0Z.	FAIL	0	0	0	3							
11295		0	0	0	4							
RV11 1/2W	AV	+0.26										
3PC	SPAN	+0.97										
250K Ω		+0.01										
11108	FAIL	0										
	AV											
	SPAN											
	FAIL											
	AV											
	SPAN											
	FAIL											
	AV											
	SPAN											
	FAIL											
	AV											
	SPAN											
	FAIL											
	AV											
	SPAN											
	FAIL											
	AV											
	SPAN											
	FAIL											

3-303-1

PREPARED BY BK, JW

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APPROVED BY

TITLE

PRE-PRODUCTION TESTS

RESISTANCE & SPEC DATA NO.		DC RESISTANCE				TORQUE CZ IN	DIEL STRENGTH	ACCEL. ERATION	SHOCK	HI FREQUENCY VIBRATION		LOW TEMP STORAGE & OP	
		$\pm 5\%$ NOM	$\pm 10\%$ NOM	70K 150K 250K	50K 125K 250K					$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
		R _T Ω	MIN MAX % OF R _T	R _{MIN} Ω	R _{MAX} Ω					% OR TOTAL	% OR TRANSIENT	% OR STOR	% OR OP
RV12 70K Ω	AV	73651	50.61	0.71	716	5.0	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	76410	58.7	1.47	1963	5.5		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	71310	45.74	0.41	46	4.5		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11114	AV	2	4	1	4	3	4	0	4	0	4	0	4
RV11 1PC 350K Ω	AV	353.92K	44.6	972.2	172.7	1.5	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	367.97K	56.7	4859.	863	1.7		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	339.97K	47.6	.41	.38	1.3		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11292	AV	1	5	1	5	0	5	0	5	0	5	0	5
RV11 3PC 250K Ω	AV	263.19K	51.1	20.39	2.52	1.3	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	272.12K	59.7	19.9	6.7	1.3		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	255.17K	49.0	.61	.31	1.2		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11115	AV	1	3	1	3	0	3	0	3	0	3	0	3
RV12 70K Ω	AV	11.77	10.5	3.07	109	2.2	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	75.370	51.61	11.55	426	4.5		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	71.900	48.90	1.25	29.6	2.0		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11112	AV	1	4	1	4	0	4	0	4	0	4	0	4
RV11 1PC 350K Ω	AV	348.79K	47.16	34.6	437.9	1.9	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	364.32K	52.3	137	2187	2.2		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	272.96K	44.1	.43	.40	1.6		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11293	AV	1	5	1	5	0	5	0	5	0	5	0	5
RV11 3PC 250K Ω	AV	256.7K	49.5	401.5	3.11	1.3	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	266.94K	51.3	832.4	4.7	1.5		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	243.37K	45.1	.24	.25	1.2		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11113	AV	1	3	1	3	0	3	0	3	0	3	0	3
RV12 70K Ω	AV	71770	51.91	5.40	108	4.44	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	72920	55.25	10.40	206	5.25		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	69000	48.42	5.33	11.4	5.25		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11116	AV	0	4	1	4	0	4	0	4	0	4	0	4
RV11 1PC 350K Ω	AV	253.84K	41.9	1.26	1.55	1.5	NO BREAKDOWN	$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	SPAN	269.54K	55.5	1.00	.79	1.6		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
	FAIL	249.76K	49.3	.53	.77	1.4		$\pm 3\%$	$\pm 2\%$	$\pm 2\%$	$\pm 10\%$	$\pm 2\%$	$\pm 3\%$
11117	AV	1	3	1	3	0	3	0	3	0	3	0	3
	SPAN												
	FAIL												
	AV												
	SPAN												
	FAIL												
	AV												
	SPAN												
	FAIL												

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DATE 9-18-61

FREQUENCY VIBRATION		TEMP STORAGE & OPER.		TEMP CYCLE	SALT SPRAY
1%	±10%	±2%	±3%	±3%	
R	%DR	%DR	%DR	%DR	
13	±0.79				
02	+1.03				
10	-1.11				
4	0				
27	±0.39				
30	+0.66				
	-0.70				
5	0				
13	±0.69				
04	+0.98				
21	-0.42				
2	0				
		+0.15	+0.37	+0.84	
		+0.31	+0.94	+1.14	
		+0.02	+0.25	+0.11	
		0	0	0	
		±0.11	±0.49	+0.84	
		+0.15	+0.35	+1.5	
		-0.11	-0.15	+0.4	
		0	0	0	
		±0.06	±0.39	+1.0	
		+0.02	+1.84	+1.5	
		-0.11	-0.21	+0.6	
		0	0	0	

* SALT SPRAY MECHANICALLY OPERATIVE; SOME CORROSION AT BUSHINGS & TERMINALS

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TABLE VII

MOISTURE TESTS, UNHOUSED RVII ELEMENTS
10 Cycles

Group No.	Termination of Material and Configuration	Original	Protective Film	" % Δ R Ave.	Span	Failure Rate ($\geq \pm 5\%$)
		Resistance Span. \times				
1	VZA + VLS, STD. SPRAY	560K to 735K	DC200. 1000CS 50% TOLUOL	+4.91	+0.47 to +25.1	2/10
2	VZA + VLS, STD. SPRAY	600K to 700K	DC3	+6.45	+1.0 to +26.3	2/9
3	VZA + VLS, STD. SPRAY	590K to 670K	TEFLON. rubbed on	+2.3	+1.3 to +5.0	1/8
4	VZA + VLS, STD. SPRAY	570K to 680K	DC200. 0.65CS	+2.48	+1.8 to +4.2	0/9
5	VZA + VLS, STD. SPRAY	590K to 690K	DESICOTE	+2.07	+0.95 to +4.7	0/10
6	VZA + VLS, STD. SPRAY	535K to 635K	NONE	± 3.27	-0.75 to +17.2	1/10
7	VZA only. curved hop off	315K to 575K	NONE	+3.8	+1.8 to +9.2	2/10
8	VZA + VLS (epoxy added) curved hop off	275K to 760K	NONE	+2.0	+0.31 to +3.3	0/10
9	VLS (epoxy added), STD. SPRAY	310K to 865K	NONE	± 1.77	-0.6 to +3.1	0/10
10	VZA + 10K/□ ink (epoxy added) STD. SPRAY	300K to 820K	NONE	+1.92	+0.15 to +3.3	0/10

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